

$$\begin{aligned}
 & - \text{polimerbitumen. hidroizolacija } 0,4+0,4 \text{ cm} \quad 0,8 \cdot 0,1 = 0,08 \text{ kN/m}^2 \\
 & - \text{AB zid } 25 \text{ cm} \quad 0,25 \cdot 25 = 6,25 = +\text{VLT} \text{ kN/m}^2 \\
 & \quad \quad \quad [(g+\text{VLT}/\text{VLT})=1,08] (+\text{VLT}) \quad g=0,50 \text{ kN/m}^2
 \end{aligned}$$

1.12. SD 1.12: Unutarnji AB zid - mjerodavni $b_w=20 \text{ cm}$

$$\begin{aligned}
 & - \text{dvostruke gipskartonske ploče } 2 \times 1,25 \text{ cm} \quad 2,5 \cdot 0,11 = 0,28 \text{ kN/m}^2 \\
 & - \text{kamena vuna, meke ploče } 8 \text{ cm} \quad 0,08 \cdot 0,3 = 0,03 \text{ kN/m}^2 \\
 & - \text{AB zid } 20 \text{ cm} \quad 0,20 \cdot 25 = 5,0 = +\text{VLT} \text{ kN/m}^2 \\
 & \quad \quad \quad [(g+\text{VLT}/\text{VLT})=1,07] (+\text{VLT}) \quad g=0,35 \text{ kN/m}^2
 \end{aligned}$$

2. PROMJENLJIVA DJELOVANJA

2.1. PD 2.1: Snijeg

Zona snijega I: $h=120 \text{ mm}$; $\alpha=1,0\%$

$$\begin{aligned}
 & - s = \mu_1 \cdot C_e \cdot C_t \cdot s_k = 0,8 \cdot 1,0 \cdot 1,0 \cdot 1,30 \quad s=1,04 \text{ kN/m}^2 \\
 & \quad \quad \quad \text{usvojeno opterećenje (TP)} \quad s=1,25 \text{ kN/m}^2
 \end{aligned}$$

2.2. PD 2.2: Vjetar

Zona vjetra I: $v_{ref}=24,64 \text{ m/s}$; $z=5,65 \text{ m}$; $KT III$; $c_e(z)=1,65$

$$\begin{aligned}
 & - w_e = q_{ref} \cdot c_e(z_e) \cdot c_{pe} = 0,5 \cdot 1,25^{-3} \cdot 24,64^2 \cdot 1,65 \cdot c_{pe} \quad 0,63 \cdot c_{pe} \text{ kN/m}^2 \\
 & - w_i = q_{ref} \cdot c_e(z_i) \cdot c_{pi} = 0,5 \cdot 1,25^{-3} \cdot 24,64^2 \cdot 1,65 \cdot c_{pi} \quad 0,63 \cdot c_{pi} \text{ kN/m}^2 \\
 & \quad \quad \quad w_e=0,63 \cdot c_{pe} \text{ kN/m}^2 \\
 & \quad \quad \quad w_i=0,63 \cdot c_{pi} \text{ kN/m}^2
 \end{aligned}$$

2.3. PD 2.3: UO ravnog neprohodnog krova

$$\begin{aligned}
 & - \text{propisano opterećenje pri uobičajenom održavanju} \quad 0,75 \text{ kN/m}^2 \\
 & \quad \quad \quad p=0,75 \text{ kN/m}^2
 \end{aligned}$$

2.4. PD 2.4: UO - školske prostorije

$$\begin{aligned}
 & - \text{propisano uporabno opterećenje} \quad 3,00 \text{ kN/m}^2 \\
 & - \text{dodatak za pregradne zidove} \quad 0,80 \text{ kN/m}^2 \\
 & \quad \quad \quad p=3,80 \text{ kN/m}^2
 \end{aligned}$$

2.5. PD 2.5: UO - športske prostorije i dvorane

$$\begin{aligned}
 & - \text{propisano uporabno opterećenje} \quad 5,00 \text{ kN/m}^2 \\
 & \quad \quad \quad p=5,00 \text{ kN/m}^2
 \end{aligned}$$



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Projekt:

Pozicija:

Ulazni podaci -
konstrukcija i opterećenja

Strana:

34

Datum:

03/2009

Ulazni podaci - Opterećenje

Lista slučajeva opterećenja				
No	Naziv	pX [kN]	pY [kN]	pZ [kN]
1	SD - stalno (g)	20.40	-34.60	-97743.38
2	PD - snijeg	21.10	-35.80	-3723.53
3	PD - uporabno	0.00	0.00	-19371.00
4	SD - tlak tla bez PV	-0.53	91.23	0.00
5	SD - tlak tla sa PV	0.22	98.78	21003.30
6	SD - tlak tla od TP	-525.82	649.08	0.00
7	Komb.: I	20.40	-34.60	-97743.38
8	Komb.: I+II	41.50	-70.40	-101466.91
9	Komb.: I+III	20.40	-34.60	-117114.38
10	Komb.: I+II+III	41.50	-70.40	-120837.91
11	Komb.: I+IV	19.87	56.63	-97743.38
12	Komb.: I+II+IV	40.97	20.83	-101466.91
13	Komb.: I+III+IV	19.87	56.63	-117114.38
14	Komb.: I+II+III+IV	40.97	20.83	-120837.91
15	Komb.: I+V	20.62	64.18	-76740.07
16	Komb.: I+II+V	41.72	28.38	-80463.60
17	Komb.: I+III+V	20.62	64.18	-96111.07
18	Komb.: I+II+III+V	41.72	28.38	-99834.60
19	Komb.: I+VI	-505.42	614.48	-97743.38
20	Komb.: I+II+VI	-484.32	578.68	-101466.91
21	Komb.: I+III+VI	-505.42	614.48	-117114.38
22	Komb.: I+II+III+VI	-484.32	578.68	-120837.91
23	Komb.: I+IV+VI	-505.94	705.71	-97743.38
24	Komb.: I+II+IV+VI	-484.84	669.91	-101466.91
25	Komb.: I+III+IV+VI	-505.94	705.71	-117114.38
26	Komb.: I+II+III+IV+VI	-484.84	669.91	-120837.91
27	Komb.: I+V+VI	-505.20	713.26	-76740.07
28	Komb.: I+II+V+VI	-484.10	677.46	-80463.60
29	Komb.: I+III+V+VI	-505.20	713.26	-96111.07
30	Komb.: I+II+III+V+VI	-484.10	677.46	-99834.60
31	Komb.: 1.35xI+1.5xII+ +1.05xIII+1.35xIV+1.35xVI	-651.37	899.01	-157878.41
32	Komb.: 1.35xI+1.5xII+ +1.05xIII+1.35xV+1.35xVI	-650.37	909.20	-129523.95
33	Komb.: 1.35xI+0.75xII+1.5 xIII+1.35xIV+1.35xVI	-667.20	925.86	-163802.71
34	Komb.: 1.35xI+0.75xII+1.5 xIII+1.35xV+1.35xVI	-666.19	936.05	-135448.25
35	Komb.: 1.35xI+1.5xII+ +1.05xIII+1.35xIV+VI	-467.34	671.83	-157878.41
36	Komb.: I+1.5xII+1.05xIII+ +1.35xIV+1.35xVI	-658.51	911.12	-123668.22
37	Komb.: 1.35xI+1.5xII+ +1.05xIII+V+1.35xVI	-651.19	867.08	-157878.41
38	Komb.: 1.35xI+1.5xII+ +1.05xIII+1.35xV+VI	-466.33	682.02	-129523.95
39	Komb.: I+1.5xII+1.05xIII+ +1.35xV+1.35xVI	-657.51	921.31	-95313.76
40	Komb.: 1.35xI+1.5xII+ +1.05xIII+V+1.35xVI	-650.44	874.62	-136875.10
41	Komb.: 1.35xI+0.75xII+1.5 xIII+1.35xV+VI	-482.16	708.87	-135448.25
42	Komb.: 1.35xI+0.75xII+1.5 xIII+1.35xIV+VI	-483.16	698.68	-163802.71
43	Komb.: 1.35xI+0.75xII+1.5 xIII+V+1.35xVI	-666.27	901.47	-142799.40
44	Komb.: I+0.75xII+1.5xIII+ +1.35xV+1.35xVI	-673.33	948.16	-101238.06
45	Komb.: I+0.75xII+1.5xIII+ +1.35xIV+1.35xVI	-674.34	937.97	-129592.52
46	Komb.: 1.35xI+0.75xII+1.5 xIII+IV+1.35xVI	-667.01	893.93	-163802.71
47	Komb.: I+1.5xII+1.05xIII+ +1.35xV+VI	-473.47	694.13	-95313.76
48	Komb.: I+1.5xII+1.05xIII+V+ +1.35xVI	-657.58	886.73	-102664.92
49	Komb.: I+1.5xII+1.05xIII+ +IV+1.35xVI	-658.33	879.19	-123668.22
50	Komb.: 1.35xI+1.5xII+ +1.05xIII+IV+VI	-467.15	639.90	-157878.41
51	Komb.: 1.35xI+1.5xII+ +1.05xIII+V+VI	-466.41	647.45	-136875.10
52	Komb.: I+1.5xII+1.05xIII+ +1.35xIV+VI	-474.48	683.94	-123668.22
53	Komb.: 1.35xI+0.75xII+1.5 xIII+V+VI	-482.23	674.30	-142799.40
54	Komb.: I+0.75xII+1.5xIII+V+ +1.35xVI	-673.41	913.58	-108589.22
55	Komb.: 1.35xI+0.75xII+1.5 xIII+IV+VI	-482.98	666.75	-163802.71
56	Komb.: I+0.75xII+1.5xIII+ +IV+1.35xVI	-674.15	906.04	-129592.52
57	Komb.: I+0.75xII+1.5xIII+ +1.35xIV+VI	-490.30	710.79	-129592.52
58	Komb.: I+0.75xII+1.5xIII+ +1.35xV+VI	-489.30	720.98	-101238.06
59	Komb.: 1.35xI+1.5xIII+ +1.35xIV+1.35xVI	-683.02	952.71	-161010.06

No	Naziv	pX [kN]	pY [kN]	pZ [kN]
60	Komb.: 1.35xI+1.5xIII+ +1.35xV+1.35xVI	-682.02	962.90	-132655.60
61	Komb.: 1.35xI+ +1.5xII+1.35xIV+1.35xVI	-651.37	899.01	-137538.86
62	Komb.: 1.35xI+1.5xII+ +1.35xV+1.35xVI	-650.37	909.20	-109184.40
63	Komb.: I+1.5xII+1.05xIII+V+VI	-473.55	659.56	-102664.92
64	Komb.: I+1.5xII+1.05xIII+ +IV+VI	-474.29	652.01	-123668.22
65	Komb.: I+0.75xII+1.5xIII+ +IV+VI	-490.12	678.86	-129592.52
66	Komb.: I+0.75xII+1.5xIII+V+VI	-489.37	686.41	-108589.22
67	Komb.: 1.35xI+1.5xIII+V+ +1.35xVI	-682.09	928.32	-140006.76
68	Komb.: I+1.5xII+1.35xIV+ +1.35xVI	-658.51	911.12	-103328.67
69	Komb.: 1.35xI+1.5xII+IV+ +1.35xVI	-651.19	867.08	-137538.86
70	Komb.: 1.35xI+ +1.5xII+1.35xIV+VI	-467.34	671.83	-137538.86
71	Komb.: I+1.5xIII+1.35xIV+ 1.35xVI	-690.16	964.82	-126799.88
72	Komb.: I+1.5xII+1.35xV+ +1.35xVI	-657.51	921.31	-74974.21
73	Komb.: I+1.5xIII+1.35xV+ +1.35xVI	-689.16	975.01	-98445.42
74	Komb.: 1.35xI+1.5xIII+ +1.35xV+VI	-497.98	735.72	-132655.60
75	Komb.: 1.35xI+1.5xII+V+ +1.35xVI	-650.44	874.62	-116535.55
76	Komb.: 1.35xI+1.5xIII+ +1.35xIV+VI	-498.99	725.53	-161010.06
77	Komb.: 1.35xI+1.5xIII+ +IV+1.35xVI	-682.84	920.78	-161010.06
78	Komb.: 1.35xI+1.5xII+ +1.35xV+VI	-466.33	682.02	-109184.40
79	Komb.: I+1.5xII+IV+1.35xVI	-658.33	879.19	-103328.67
80	Komb.: 1.35xI+1.5xIII+IV+VI	-498.80	693.60	-161010.06
81	Komb.: 1.35xI+1.5xIII+V+VI	-498.06	701.15	-140006.76
82	Komb.: 1.35xI+1.5xII+IV+VI	-467.15	639.90	-137538.86
83	Komb.: I+1.5xII+1.35xIV+VI	-474.48	683.94	-103328.67
84	Komb.: I+1.5xIII+1.35xIV+VI	-506.13	737.64	-126799.88
85	Komb.: I+1.5xIII+IV+1.35xVI	-689.98	932.89	-126799.88
86	Komb.: I+1.5xII+V+1.35xVI	-657.58	886.73	-82325.37
87	Komb.: 1.35xI+1.5xII+V+VI	-466.41	647.45	-116535.55
88	Komb.: I+1.5xIII+1.35xV+VI	-505.12	747.83	-98445.42
89	Komb.: I+1.5xIII+V+1.35xVI	-689.23	940.43	-105796.57
90	Komb.: I+1.5xII+1.35xV+VI	-473.47	694.13	-74974.21
91	Komb.: I+1.5xIII+IV+VI	-505.94	705.71	-126799.88
92	Komb.: I+1.5xII+IV+VI	-474.29	652.01	-103328.67
93	Komb.: I+1.5xII+V+VI	-473.55	659.56	-82325.37
94	Komb.: I+1.5xIII+V+VI	-505.20	713.26	-105796.57
95	Komb.: 1.35xI+1.35xIV+1.3 5xVI	-683.02	952.71	-131953.56
96	Komb.: 1.35xI+ +1.35xV+1.35xVI	-682.02	962.90	-103599.10
97	Komb.: 1.35xI+V+1.35xVI	-682.09	928.32	-110950.26
98	Komb.: 1.35xI+1.35xV+VI	-497.98	735.72	-103599.10
99	Komb.: I+1.35xV+1.35xVI	-689.16	975.01	-69388.92
100	Komb.: 1.35xI+IV+1.35xVI	-682.84	920.78	-131953.56
101	Komb.: 1.35xI+1.35xIV+VI	-498.99	725.53	-131953.56
102	Komb.: I+1.35xIV+1.35xVI	-690.16	964.82	-97743.38
103	Komb.: I+IV+1.35xVI	-689.98	932.89	-97743.38
104	Komb.: I+V+1.35xVI	-689.23	940.43	-76740.07
105	Komb.: I+1.35xV+VI	-505.12	747.83	-69388.92
106	Komb.: 1.35xI+IV+VI	-498.80	693.60	-131953.56
107	Komb.: 1.35xI+V+VI	-498.06	701.15	-110950.26
108	Komb.: I+1.35xIV+VI	-506.13	737.64	-97743.38
109	Komb.: I+V+VI	-505.20	713.26	-76740.07
110	Komb.: I+IV+VI	-505.94	705.71	-97743.38



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Projekt:

Strana:

42

Pozicija:

P203

Datum:

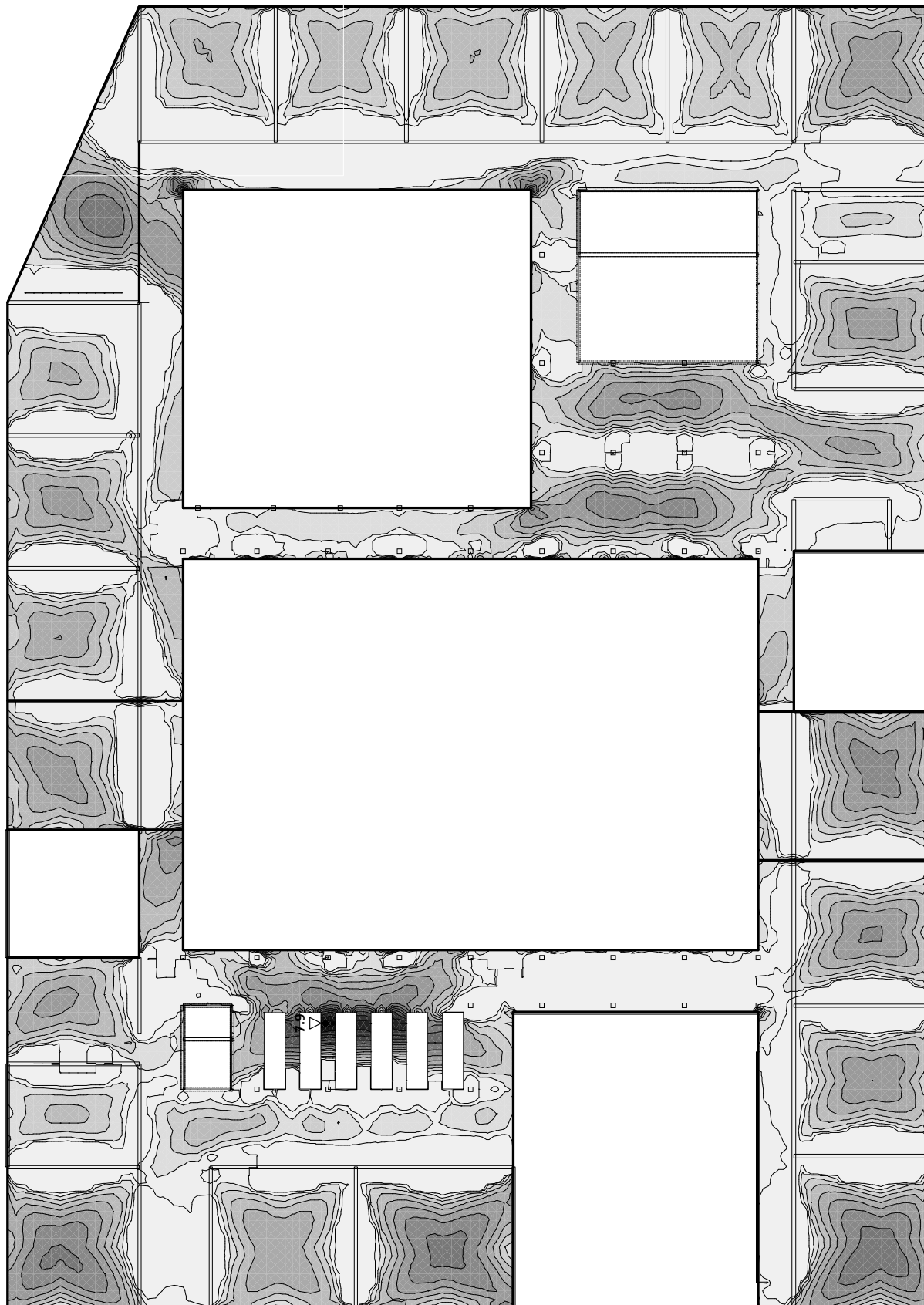
03/2009

Dimenzioniranje (beton)

Aa - d.zona - Pravac 1 [cm²/m]



Mjerodavno opterećenje: [Stalna ili prolazna KO] 31-110
EUROCODE, C 30/37, B 500B, a=3.50 cm



Nivo: [3.75 m]

Aa - d.zona - Pravac 1 - max Aa1,d= 7.9 cm²/m



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Projekt:

Strana:

43

Pozicija:

P203

Datum:

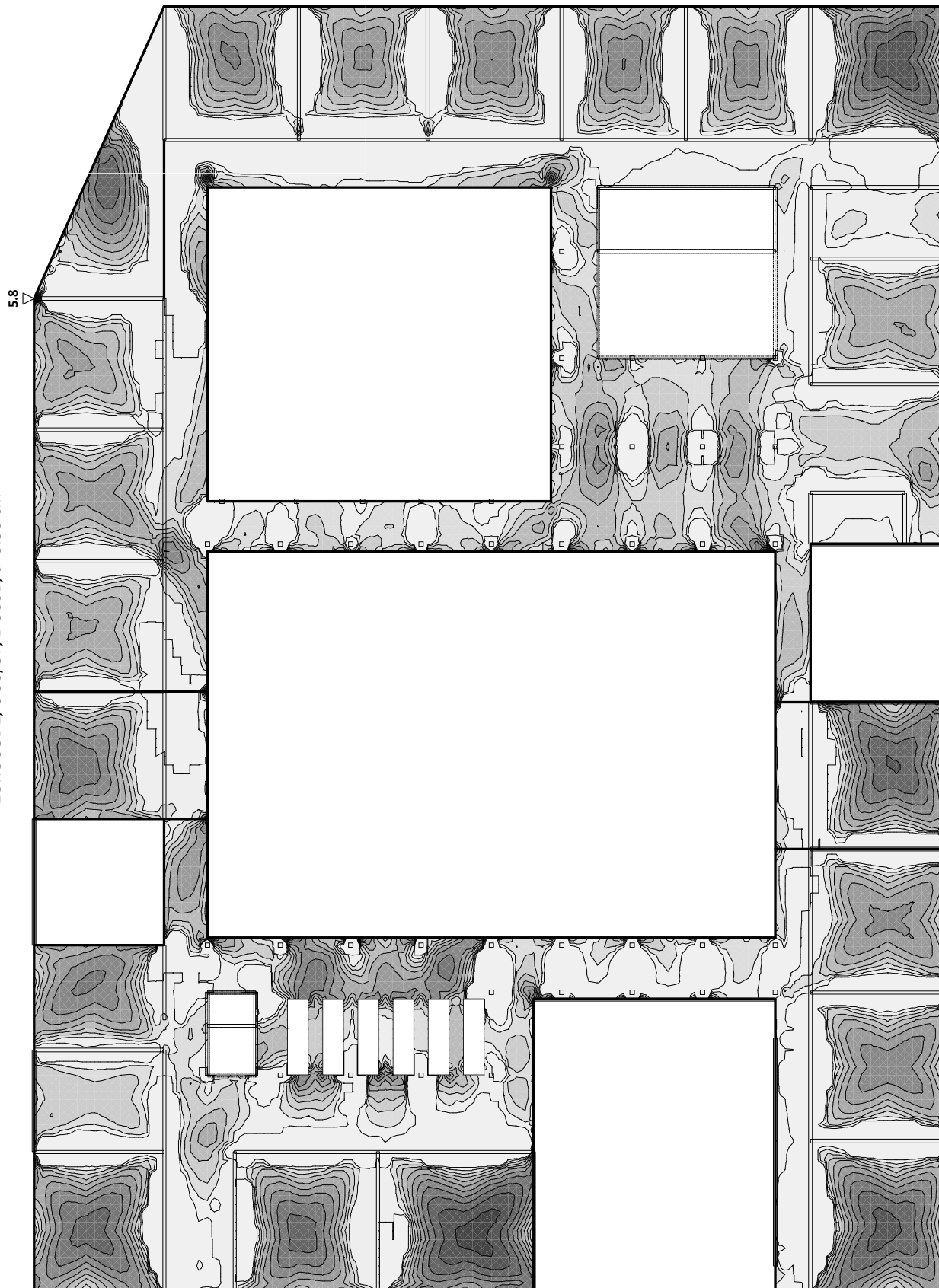
03/2009

Dimenzioniranje (beton)

Aa - d.zona - Pravac 2 [cm²/m]



Mjerodavno opterećenje: [Stalna ili prolazna KO] 31-110
EUROCODE, C 30/37, B 500B, a=3.50 cm



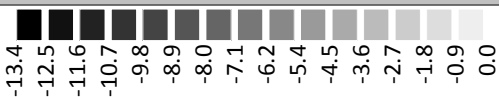
Nivo: [3.75 m]

Aa - d.zona - Pravac 2 - max Aa_{2,d} = 5.8 cm²/m

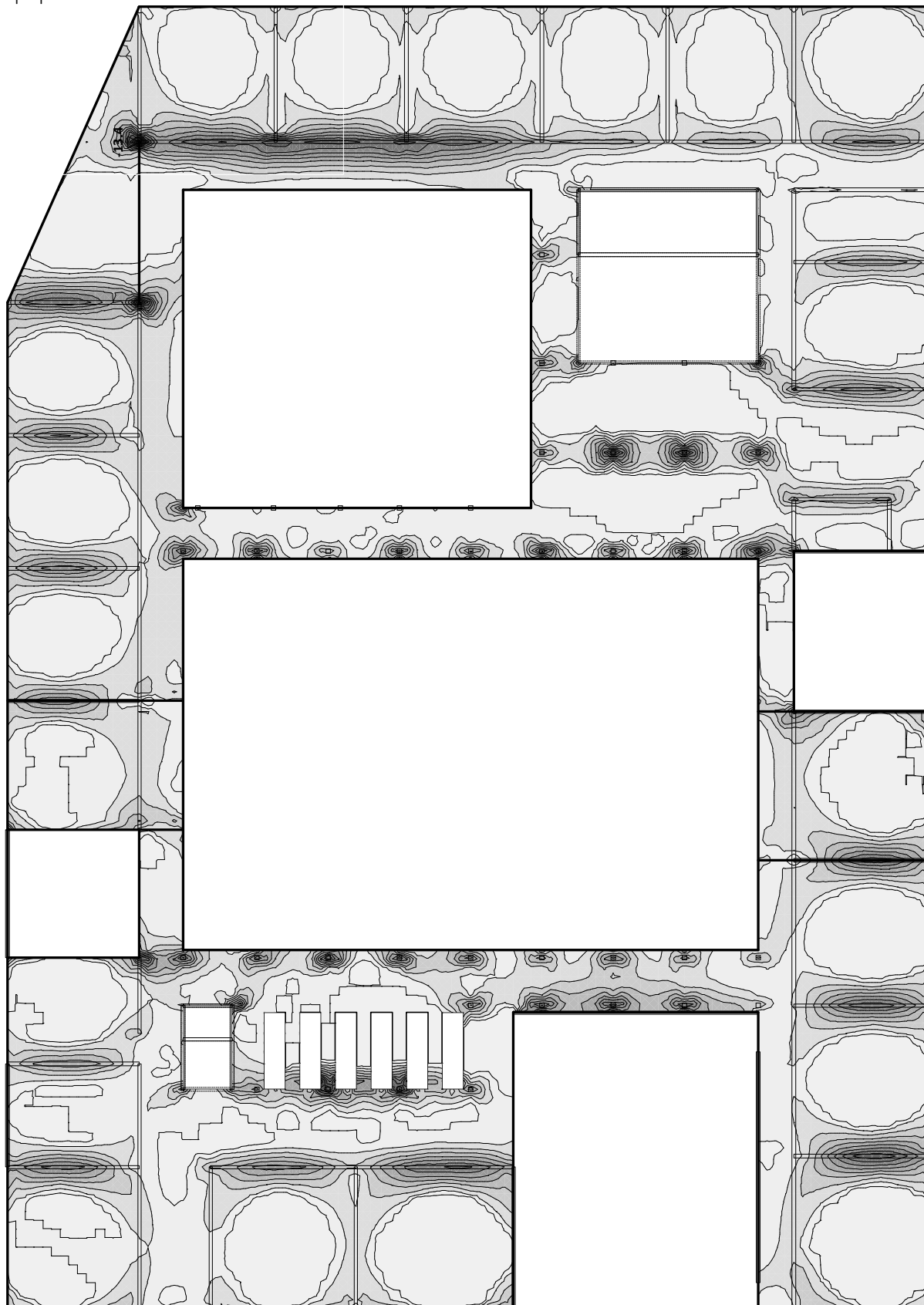


Dimenzioniranje (beton)

Aa - g.zona - Pravac 1 [cm²/m]



Mjerodavno opterećenje: [Stalna ili prolazna KO] 31-110
 EUROCODE, C 30/37, B 500B, a=3.50 cm



Nivo: [3.75 m]

Aa - g.zona - Pravac 1 - max Aa1,g= -13.4 cm²/m



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Projekt:

Strana:

45

Pozicija:

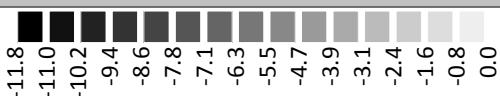
P203

Datum:

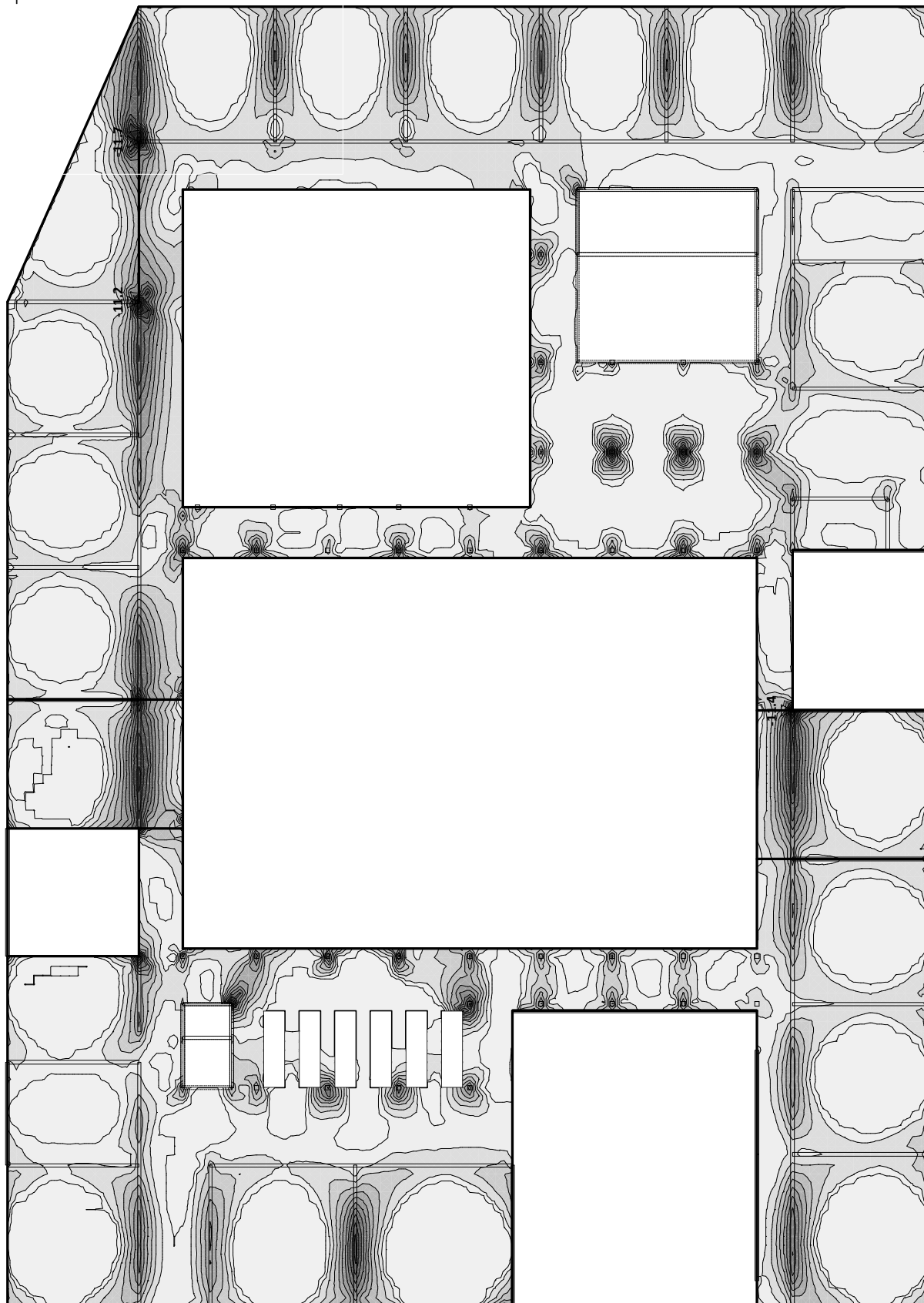
03/2009

Dimenzioniranje (beton)

Aa - g.zona - Pravac 2 [cm²/m]



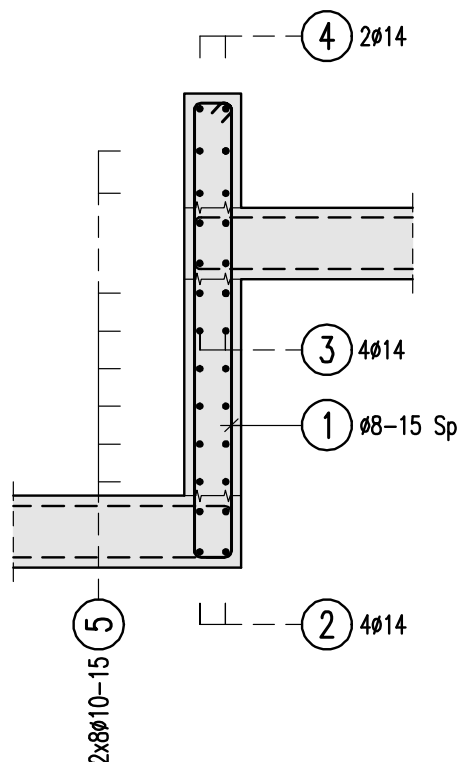
Mjerodavno opterećenje: [Stalna ili prolazna KO] 31-110
EUROCODE, C 30/37, B 500B, a=3.50 cm



Nivo: [3.75 m]

Aa - g.zona - Pravac 2 - max Aa2,g= -11.7 cm²/m





Poz. Z102: Unutarnji AB zidovi podruma $b_w=20$ cm

Materijali: C 25/30, B 500B, RI XC1, $c_{nom} = 25$ mm, $d_g \leq 32$ mm

Usvojena minimalna armatura:

$$A_{sv,min} = 0,0015 \cdot A_c = 0,0015 \cdot 20 \cdot 100 = 3,00 \text{ cm}^2/\text{m}' \text{ u krajnjih } L/10$$

$$A_{sv,min} = 0,0020 \cdot A_c = 0,0020 \cdot 20 \cdot 100 = 4,00 \text{ cm}^2/\text{m}' \text{ u sredini}$$

$$A_{sh,min} = 0,0020 \cdot A_c = 0,0020 \cdot 20 \cdot 100 = 4,00 \text{ cm}^2/\text{m}'$$

Q335 obostrano

4Ø16 na mjestima križanja zidova i oslanjanja greda

2Ø16 oko otvora

4Ø16 na slobodnim rubovima

Poz. Z103: Unutarnji AB zid podruma $b_w=25$ cm

Materijali: C 25/30, B 500B, RI XC1, $c_{nom} = 25$ mm, $d_g \leq 32$ mm

Usvojena minimalna armatura:

$$A_{sv,min} = 0,0015 \cdot A_c = 0,0015 \cdot 25 \cdot 100 = 3,75 \text{ cm}^2/\text{m}' \text{ u krajnjih } L/10$$

$$A_{sv,min} = 0,0020 \cdot A_c = 0,0020 \cdot 25 \cdot 100 = 5,00 \text{ cm}^2/\text{m}' \text{ u sredini}$$

$$A_{sh,min} = 0,0020 \cdot A_c = 0,0020 \cdot 25 \cdot 100 = 5,00 \text{ cm}^2/\text{m}'$$

Q385 obostrano

4Ø16 na mjestima križanja zidova i oslanjanja greda

2Ø16 oko otvora

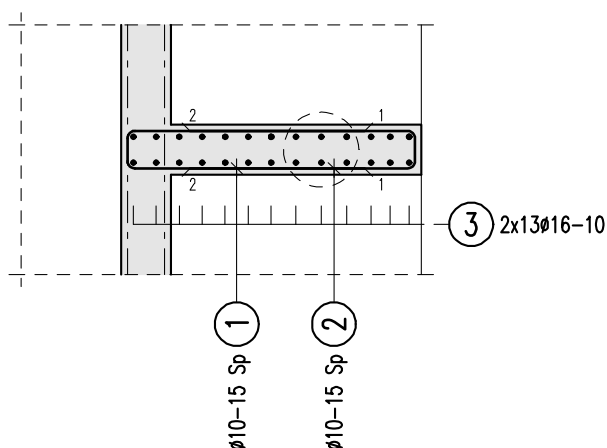
4Ø16 na slobodnim rubovima

Poz. Z104: Unutarnji AB zidovi podruma $b_w=20$ cm

Materijali: C 25/30, B 500B, RI XC1, $c_{nom} = 25$ mm, $d_g \leq 32$ mm

Usvojena armatura:

uzdužna: 13 $\emptyset$ 16-10 obostrano
poprečna: $\emptyset$ 10-15 cm spone
na mjestu oslanjanja stupa: 2x3 $\emptyset$ 16



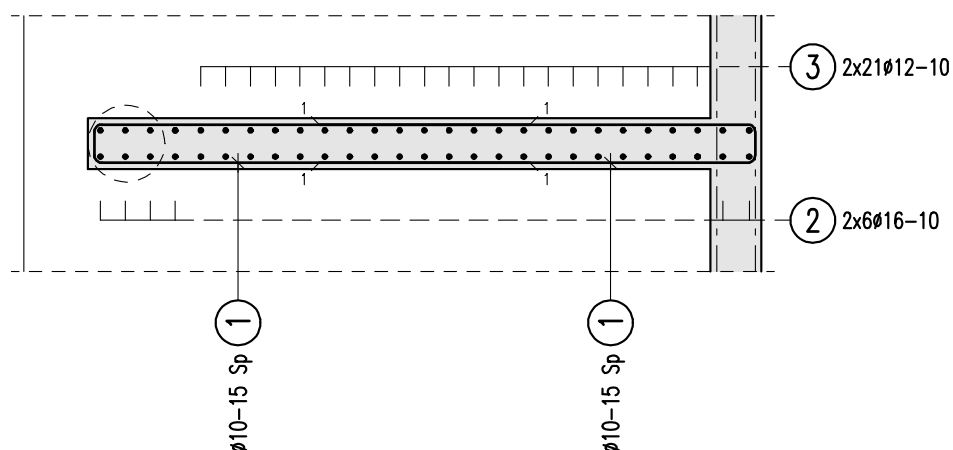
Poz. Z105: Unutarnji AB zidovi podruma $b_w=20$ cm

Materijali: C 25/30, B 500B, RI XC1, $c_{nom} = 25$ mm, $d_g \leq 32$ mm

Usvojena armatura:

uzdužna: 2x4 $\emptyset$ 16 slobodni rub, 2x2 $\emptyset$ 16 križanje zidova
 $\emptyset$ 12-10 u sredini obostrano
poprečna: $\emptyset$ 10-15 cm spone
na mjestu oslanjanja stupa: 2x3 $\emptyset$ 16

Skica armature:





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Projekt:

Strana:

87

Pozicija:

Z101

Datum:

03/2009

Poz. Z101: Vanjski AB zidovi podruma $b_w=30$ cm

1. Statički sistem

Vidi kompjuterski proračun

2. Materijalne i geometrijske karakteristike

Materijali: C 30/37, B 500B, RI XC4/XF1, $c_{nom} = 35$ mm, $d_g \leq 32$ mm
Poprečni presjek: $b_w=30$ cm

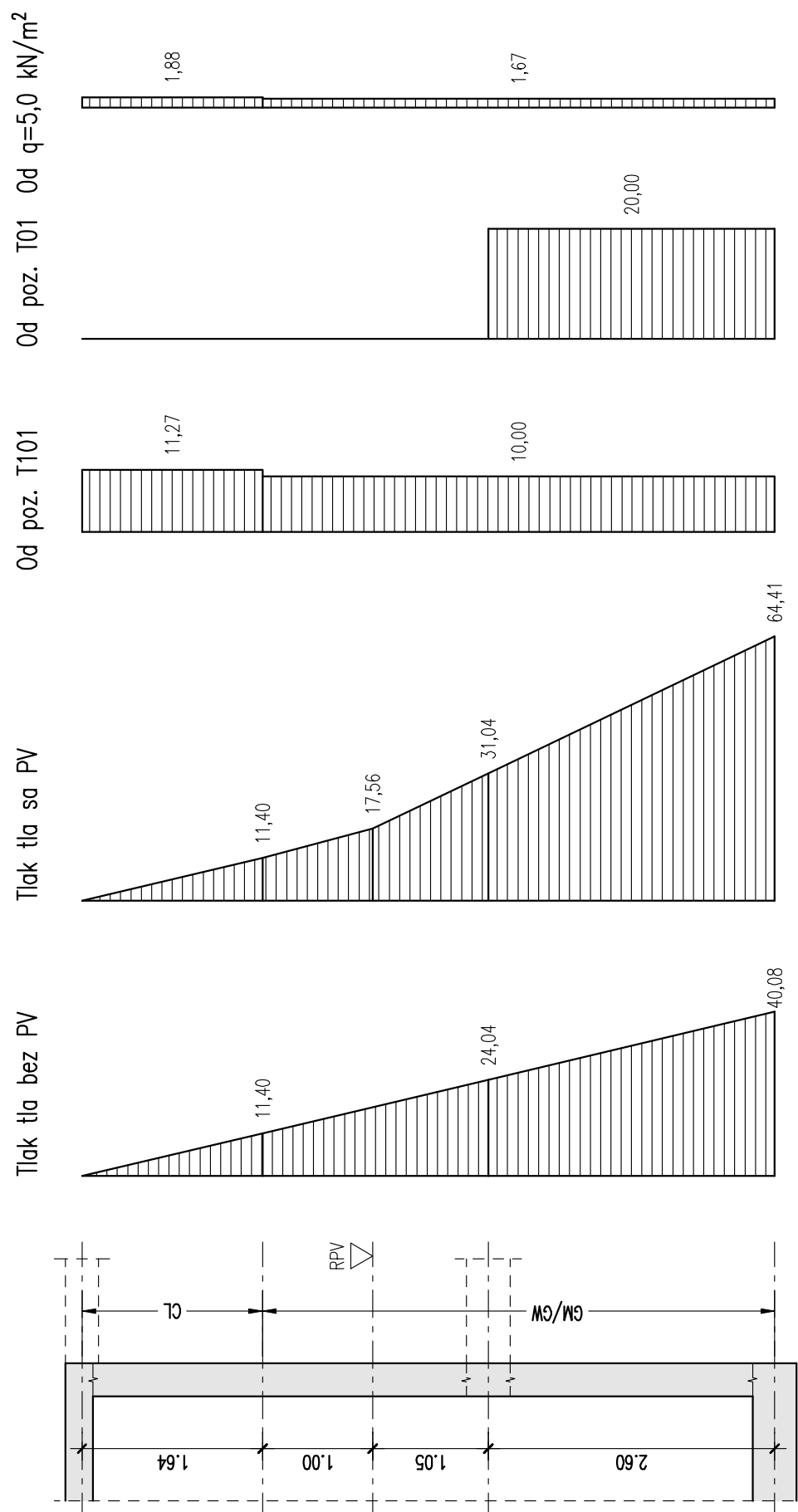
3. Opterećenje

Vidi kompjuterski proračun

		SD	PD	ID
SD 1.8	(+VLT) [kN/m ²]	0,20		
SD 1.9	(+VLT) [kN/m ²]	0,40		
SD,PD	objekt, generirano proračunom [kN/m']	VKP	VKP	
h=0,0	Tlak tla bez podzemne vode = $\gamma \cdot h \cdot K_{agh}$			
h=1,64	18,5·1,64·0,3757 [kN/m ²]	11,40		
h=3,69	11,40+18,5·2,05·0,3333 [kN/m ²]	24,04		
z=6,29	24,04+18,5·2,60·0,3333 [kN/m ²]	40,08		
h=0,0	TT sa podzemnom vodom = $\gamma' \cdot h \cdot K_{agh} + \gamma_v \cdot h$			
h=1,64	18,5·1,64·0,3757 [kN/m ²]	11,40		
h _{PV} =2,64	11,40+18,5·1,0·0,3333 [kN/m ²]	17,56		
h=3,69	17,56+8,5·1,05·0,3333+10,0·1,05 [kN/m ²]	31,04		
h=6,29	31,04+8,5·2,60·0,3333+10,0·2,60 [kN/m ²]	64,41		
h=0,0	Tlak tla od poz. T101 = $q \cdot K_{agh}$			
h=1,64	30,0·0,3757 [kN/m ²]	11,27		
h=6,29	30,0·0,3333 [kN/m ²]	10,00		
h=3,69	Tlak tla od poz. T01 = $q \cdot K_{agh}$			
h=6,29	60,0·0,3333 [kN/m ²]	20,00		
h=0,0	Tlak tla od $q=5,0$ kN/m ² = $q \cdot K_{agh}$			
h=1,64	5,0·0,3757 [kN/m ²]	1,88		
h=6,29	5,0·0,3333 [kN/m ²]	1,67		

4. Rezne sile

Vidi kompjuterski proračun



5. Dimenzioniranje

Potrebna minimalna armatura:

$$A_{sv,min} = 0,0015 \cdot A_c = 0,0015 \cdot 30 \cdot 100 = 4,50 \text{ cm}^2/\text{m}' \text{ u krajnjih L/10}$$

$$A_{sv,min} = 0,0020 \cdot A_c = 0,0020 \cdot 30 \cdot 100 = 6,00 \text{ cm}^2/\text{m}' \text{ u sredini}$$

$$A_{sh,min} = 0,0020 \cdot A_c = 0,0020 \cdot 30 \cdot 100 = 6,00 \text{ cm}^2/\text{m}'$$

Osnovna armatura iz uvjeta ograničenja širine pukotina pri oslobađanju hidratacijske topline, **CEM I / 32,5 N**, centrični vlak, $w_g \leq 0,3 \text{ mm}$: **Q636 (ø9-10 cm) d+g**. Dodatnu armaturu usvojiti prema rezultatima proračuna potrebne armature.

U tekstualnom dijelu dokumentacije prikazani su rezultati potrebne armature samo za pojedine, karakteristične i najviše opterećene zidove. U digitalnom obliku glavnog projekta dati su rezultati za sve zidovi.

Usvojena armatura:

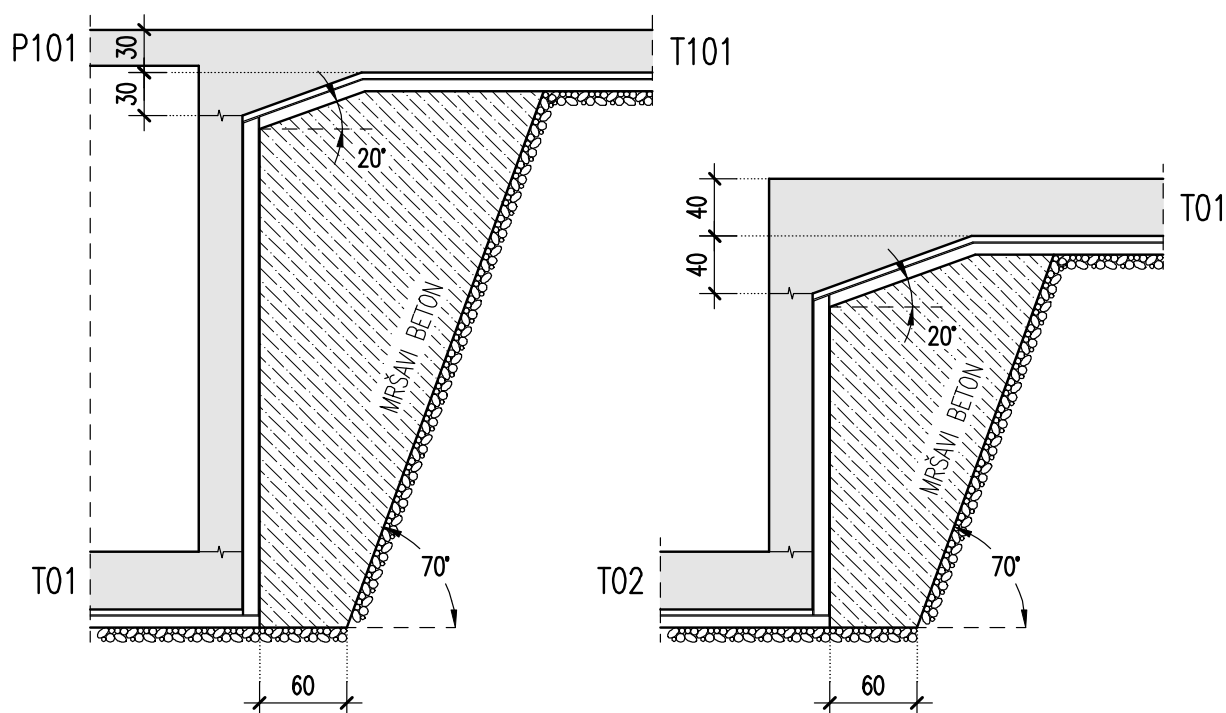
Q636 obostrano

4ø16 na mjestima križanja zidova i oslanjanja greda

2ø16 oko otvora

4ø16 na slobodnim rubovima

Zidove poz. **Z101** koji se nalaze ispod temeljnih ploča poz. **T01** i **T101** podbetonirati mršavim betonom prema skici:





PLAN POZICIJA TEMELJA
M 1:100

